# SIZE SELECTION - CLUTCH TORQUE

The basic relationship between TORQUE, MOTOR POWER Pin kW and SPEED :  $M = \frac{9550 \times P}{RPM} = Nm$  provides a torque value

for normal full load running of a machine. The Clutch must, however, have a reserve of torque for intermittent over-loads and a factor of safety must be allowed so that torque is based on M =  $\frac{K \times 9550 \times P}{RPM}$  = Nm where K is the safety over-load

factor and M the static torque of the Clutch. For electric motor drives (3 phase squirrel cage) the pull out torque of the motor is usually about 2.5 × Full Load Torque and this factor of 2.5 may be used for K for many machines driven by electric motors and give an adequate reserve of clutch torque. The factor can, of course, be safely reduced, say to 1.5 for such loads as centrifugal pumps or light conveyors where only small overloads can occur. A higher factor for K may, however, be necessary if the machine requires the full overload torque before it attains full speed.

The reason for this is that at the instant of engagement and during acceleration of the machine the Clutch is developing less than its normal static torque since it is actually slipping until it has brought the machine up to the same speed as the driving shaft. The speed/torque curves appearing on each data sheet enable a suitable safety factor to be adopted. Special consideration must be given when dealing with:

(a) Machines which incorporate flywheels to deal with high peak torque, i.e. presses and guillotines.

(b) Machines with high inertias which need to be started and stopped very frequently. For this duty the heat dissipation during each start must be calculated to ensure that it comes within the thermal capacity of the Clutch.

For these applications we suggest that details are passed to our local engineer or head office in order that a suitable size can be recommended.

# BRAKE TORQUE

The selection of a Brake to stop a machine in a given time may be determined from the following formula :  $Ma = \frac{J n}{0.55t}$ 

where Ma = Torque in Nm to stop the machine in time t seconds.

J = Weight of rotating masses x effective radius squared expressed kgm<sup>2</sup>. n = initial speed in RPM. It will be noted from the speed/torque curves that the Brake Torque will automatically increase as the machine is slowed down. If Mis therefore taken as the value at the initial speed then the Brake will have a reserve of torque for the job. As in the case of Clutches, we suggest that details are passed to us for size recommendation where machines have high energy or inertias, i.e. Centrifuges, or where the machine is started and stopped very frequently.

## **SELECTION TABLE**

Allowing for 250% torque overloads after Clutch has brought load to full speed.

|          | SHAFT SPEED AT CLUTCH IN R.P.M. |     |            |     |       |     |     |     |     |      |      |      |      |      |      |      |      |      |
|----------|---------------------------------|-----|------------|-----|-------|-----|-----|-----|-----|------|------|------|------|------|------|------|------|------|
| Motor kW | 100                             | 200 | 300        | 400 | 500   | 600 | 700 | 800 | 900 | 1000 | 1250 | 1440 | 1750 | 2000 | 2500 | 2800 | 3000 | 4000 |
| 0.015    | 250                             | 250 | 250        | 175 | 175   | 175 | 175 | 175 | 175 | 175  | 175  | 175  | 175  | 175  | 175  | 175  | 175  | 175  |
| 0.037    | 365                             | 250 | 250        | 250 | 250   | 250 | 250 | 175 | 175 | 175  | 175  | 175  | 175  | 175  | 175  | 175  | 175  | 175  |
| 0.06     | 400                             | 365 | 250        | 250 | 250   | 250 | 250 | 250 | 250 | 250  | 250  | 175  | 175  | 175  | 175  | 175  | 175  | 175  |
| 0.09     | 400                             | 400 | 365        | 250 | 250   | 250 | 250 | 250 | 250 | 250  | 250  | 250  | 250  | 175  | 175  | 175  | 175  | 175  |
| 0.12     | 600                             | 400 | 365        | 365 | 365   | 250 | 250 | 250 | 250 | 250  | 250  | 250  | 250  | 250  | 250  | 175  | 175  | 175  |
| 0.18     | 600                             | 400 | 400        | 400 | 365   | 365 | 365 | 250 | 250 | 250  | 250  | 250  | 250  | 250  | 250  | 250  | 250  | 175  |
| 0.25     | 600                             | 600 | 400        | 400 | 400   | 365 | 365 | 365 | 365 | 365  | 250  | 250  | 250  | 250  | 250  | 250  | 250  | 250  |
| 0.37     | 800                             | 600 | 600        | 400 | 400   | 400 | 400 | 400 | 365 | 365  | 365  | 365  | 250  | 250  | 250  | 250  | 250  | 250  |
| 0.55     | 800                             | 800 | 600        | 600 | 600   | 400 | 400 | 400 | 400 | 400  | 365  | 365  | 365  | 365  | 250  | 250  | 250  | 250  |
| 0.75     |                                 | 800 | 600        | 600 | 600   | 600 | 600 | 400 | 400 | 400  | 400  | 400  | 365  | 365  | 365  | 365  | 365  | 250  |
| 1.1      |                                 | 800 | 800        | 600 | 600   | 600 | 600 | 600 | 600 | 600  | 400  | 400  | 400  | 400  | 365  | 365  | 365  | 365  |
| 1.5      | 1                               |     | 800        | 800 | 800   | 600 | 600 | 600 | 600 | 600  | 600  | 600  | 400  | 400  | 400  | 400  | 400  | 365  |
| 2.2      |                                 |     |            | 800 | 800   | 800 | 800 | 600 | 600 | 600  | 600  | 600  | 600  | 600  | 400  | 400  | 400  | 400  |
| 3.0      |                                 |     |            |     |       |     | 800 | 800 | 800 | 800  | 800  | 600  | 600  | 600  | 600  | 600  | 600  | 400  |
| 5.5      |                                 |     | <b>6</b> 1 | HTC | u cu  | VE. |     |     |     |      | 800  | 800  | 800  | 800  | 600  | 600  | 600  | 600  |
| 7.5      |                                 |     | CL         | UTC | п ЭІ/ | LE  |     |     |     |      |      | 800  | 800  | 800  | 800  | 600  | 600  | 600  |
| 9.3      |                                 |     |            |     |       |     |     |     |     |      |      |      | 800  | 800  | 800  | 800  | 800  | 600  |
| 11.0     |                                 |     |            |     |       |     |     |     |     |      |      |      |      | 800  | 800  | 800  | 800  | 800  |

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